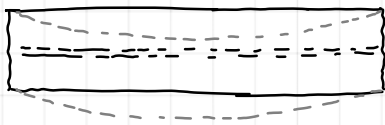
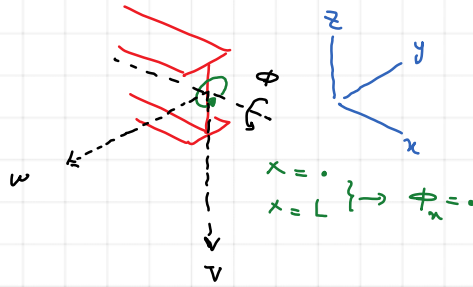
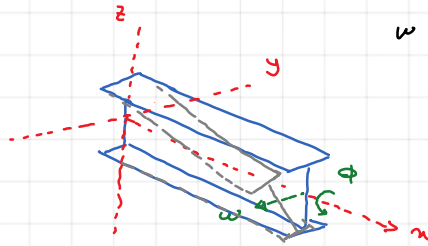
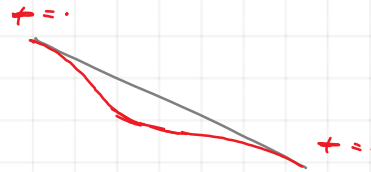


This series of videos teaches the calculation of buckling load for a simply supported beam under a distributed load. As you may noticed, Eurocode does not provide an equation for critical bending moment in lateral torsional buckling calculation.

This video presents a calculation of buckling load using total potential energy. Subsequent videos will cover buckling load calculations using Ansys and RFEM.



$w \rightarrow$  half Sin



$\phi \rightarrow$  cos

$$w(x) = A \sin\left(\frac{\pi x}{L}\right) \rightarrow$$

$$x=0 \rightarrow w(0) = 0$$

$$x=L \rightarrow w(L) = 0$$

$$x = \frac{L}{2} \rightarrow w\left(\frac{L}{2}\right) = A$$

$$\phi(x) = B \cdot \left[ \cos\left(\frac{2\pi x}{L}\right) - 1 \right] \rightarrow$$

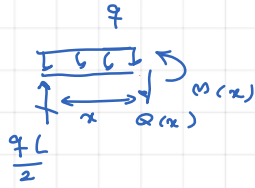
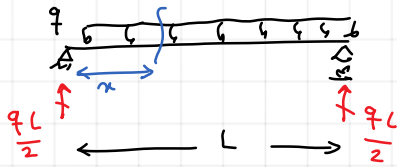
$$x=0 \rightarrow \phi(0) = 0$$

$$x=L \rightarrow \phi(L) = 0$$

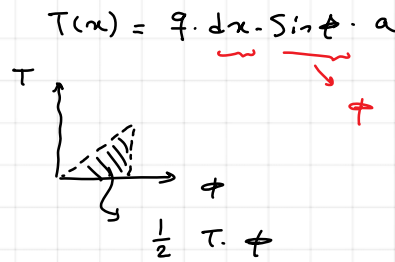
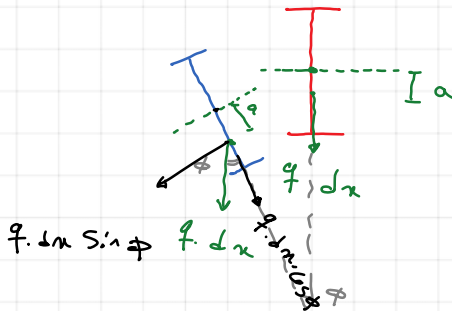
$$x = \frac{L}{2} \rightarrow \phi\left(\frac{L}{2}\right) = -B$$

$$\pi = \frac{1}{2} \int_0^L E I_z \cdot w''(x)^2 dx + \frac{1}{2} \int_0^L G I_t \cdot \phi'(x)^2 dx$$

$$+ \frac{1}{2} \int_0^L E I_w \phi''(x)^2 dx - \int_0^L (M_y(x) \phi(x))' w'(x) dx + \int_0^L \frac{1}{2} T(x) \phi(x)$$



$$M_y(x) = \frac{qL}{2} \cdot x - \frac{q \cdot x^2}{2}$$



$$\begin{aligned} \pi = & \frac{1}{2} \int_0^L E I_z \cdot \dot{w}(x)^2 dx + \frac{1}{2} \int_0^L G I_t \cdot \phi(x)^2 dx \\ & + \frac{1}{2} \int_0^L E I_w \phi(x)^2 dx - \int_0^L (M_y(x) \phi(x))' w(x) dx + \int_0^L \frac{1}{2} T(x) \phi(x) dx \end{aligned}$$

$$w(x) = A \sin\left(\frac{\pi \cdot x}{L}\right)$$

$$\phi(x) = B \left[ \cos\left(\frac{2\pi \cdot x}{L}\right) - 1 \right]$$

$$M_y(x) = \frac{qL}{2} x - \frac{q x^2}{2}$$

$$T(x) = q \cdot \phi(x) \cdot a$$

$$w(x, l, A) := A \cdot \sin\left(\frac{\pi \cdot x}{l}\right)$$

$$\phi(x, l, B) := B \cdot \left(\cos\left(\frac{2 \cdot \pi \cdot x}{l}\right) - 1\right)$$

$$M_y(x, l, q) := \frac{q \cdot l}{2} \cdot x - \frac{q \cdot x^2}{2}$$

$$T(x, l, B, q, a) := q \cdot \phi(x, l, B) \cdot a$$

$$\begin{aligned} \Pi(A, B, l, E, G, I_z, I_t, I_w, q, a) := & \frac{1}{2} \cdot \int_0^l E \cdot I_z \cdot \left(\frac{\partial^2 w(x, l, A)}{\partial x^2}\right)^2 dx + \frac{1}{2} \cdot \int_0^l G \cdot I_t \cdot \left(\frac{\partial}{\partial x} \phi(x, l, B)\right)^2 dx \\ & + \frac{1}{2} \cdot \int_0^l E \cdot I_w \cdot \left(\frac{\partial^2 \phi(x, l, B)}{\partial x^2}\right)^2 dx - \int_0^l \left(\frac{\partial}{\partial x} (M_y(x, l, q) \cdot \phi(x, l, B))\right) \cdot \left(\frac{\partial}{\partial x} w(x, l, A)\right) dx \\ & + \frac{1}{2} \cdot \int_0^l T(x, l, B, q, a) \cdot \phi(x, l, B) dx \end{aligned}$$

$$\frac{\partial}{\partial A} \Pi(A, B, l, E, G, I_z, I_t, I_w, q, a) \rightarrow \frac{I_z \cdot A \cdot E \cdot \pi^4}{2 \cdot l^3} + \frac{80 \cdot B \cdot l \cdot q}{27 \cdot \pi}$$

$$\frac{\partial}{\partial B} \Pi(A, B, l, E, G, I_z, I_t, I_w, q, a) \rightarrow \frac{8 \cdot I_w \cdot B \cdot E \cdot \pi^4}{l^3} + \frac{2 \cdot I_t \cdot B \cdot G \cdot \pi^2}{l} + \frac{3 \cdot B \cdot a \cdot l \cdot q}{2} + \frac{80 \cdot A \cdot l \cdot q}{27 \cdot \pi}$$

$$\text{Mat}(l, E, G, I_z, I_t, I_w, q, a) := \begin{bmatrix} \frac{I_z \cdot E \cdot \pi^4}{2 \cdot l^3} & \frac{80 \cdot l \cdot q}{27 \cdot \pi} \\ \frac{80 \cdot l \cdot q}{27 \cdot \pi} & \frac{8 \cdot I_w \cdot E \cdot \pi^4}{l^3} + \frac{2 \cdot I_t \cdot G \cdot \pi^2}{l} + \frac{3 \cdot a \cdot l \cdot q}{2} \end{bmatrix}$$

Profile	Area A <sub>z-z</sub> [mm <sup>2</sup> ] η=1.2	Shear area A <sub>v,y</sub> [mm <sup>2</sup> ]	Second moment of area I <sub>y</sub> [×10 <sup>6</sup> mm <sup>4</sup> ]	Radius of gyration i <sub>y</sub> [mm]	Elastic section modulus W <sub>el,y</sub> [×10 <sup>3</sup> mm <sup>3</sup> ]	Plastic section modulus W <sub>pl,y</sub> [×10 <sup>3</sup> mm <sup>3</sup> ]	Second moment of area I <sub>z</sub> [×10 <sup>6</sup> mm <sup>4</sup> ]	Radius of gyration i <sub>z</sub> [mm]	Elastic section modulus W <sub>el,z</sub> [×10 <sup>3</sup> mm <sup>3</sup> ]	Plastic section modulus W <sub>pl,z</sub> [×10 <sup>3</sup> mm <sup>3</sup> ]	Torsion constant I <sub>T</sub> [×10 <sup>3</sup> mm <sup>4</sup> ]	Torsion modulus W <sub>T</sub> [×10 <sup>3</sup> mm <sup>3</sup> ]	Warping constant I <sub>w</sub> [×10 <sup>6</sup> mm <sup>6</sup> ]	Warping modulus W <sub>w</sub> [×10 <sup>3</sup> mm <sup>4</sup> ]
HEA200	808	4000	36.92	82.8	388.6	429.5	13.36	49.8	133.6	203.8	204.3	31.43	105580	11830

$$I_z := 13.36 \cdot 10^6 \cdot \text{mm}^4$$

$$I_t := 204.3 \cdot 10^3 \cdot \text{mm}^4$$

$$I_w := 105580 \cdot 10^6 \cdot \text{mm}^6$$

$$E := 210 \text{ GPa}$$

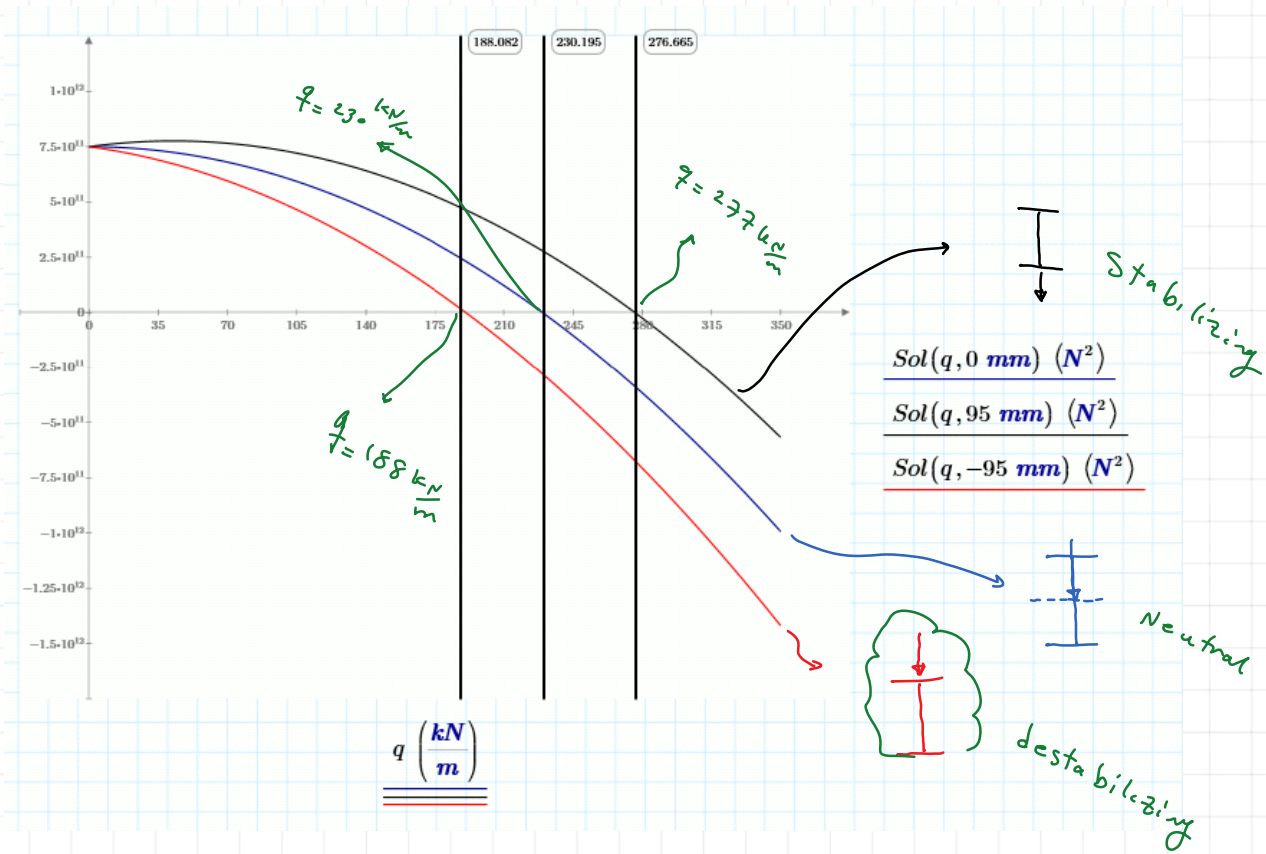
$$v := 0.3$$

$$G := \frac{E}{2(1+v)}$$

$$l := 4 \text{ m}$$

$$\text{Sol}(q, a) := \det(\text{Mat}(l, E, G, I_z, I_t, I_w, q, a))$$

$$q := 0, 0.1 \frac{\text{kN}}{\text{m}} \dots 350 \frac{\text{kN}}{\text{m}}$$



Des:  $\rightarrow M_{cr} = \frac{qL^2}{8} = \frac{188 \frac{kN}{m} \times (4m)^2}{8} = 376 \text{ kN}\cdot\text{m}$

Neu:  $\rightarrow M_{cr} = \frac{230 \frac{kN}{m} \times (4m)^2}{8} = 460 \text{ kN}\cdot\text{m}$

Sta:  $\rightarrow M_{cr} = \frac{277 \frac{kN}{m} \times (4m)^2}{8} = 554 \text{ kN}\cdot\text{m}$