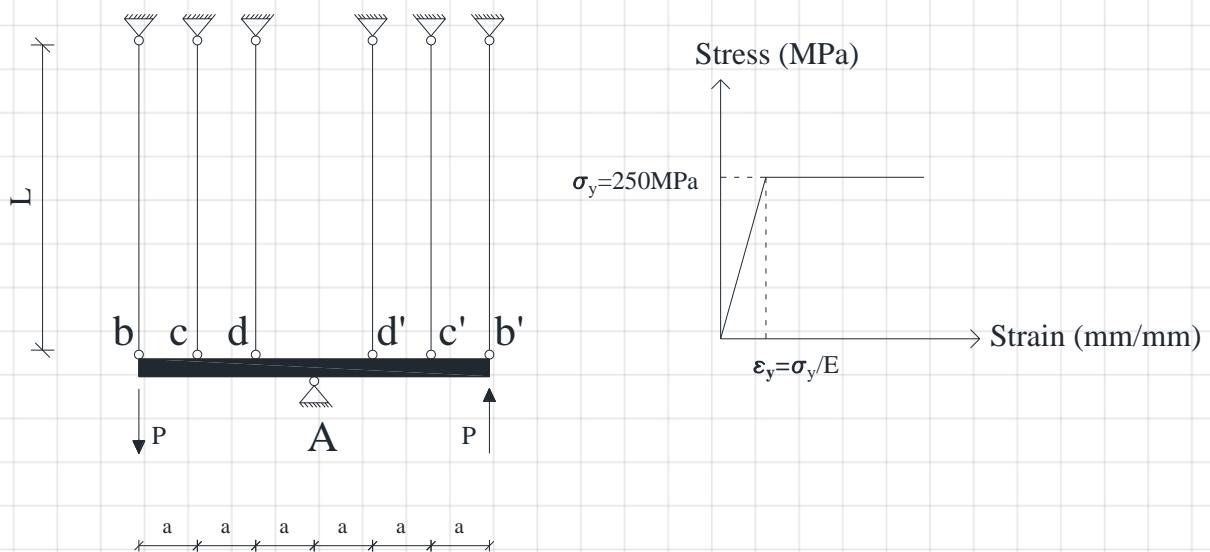


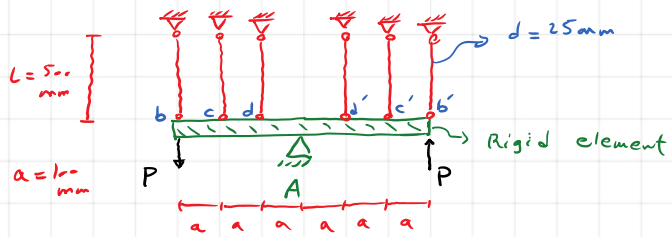
This video teaches us how to determine the elastic and plastic load for a rigid element connected to deformable bars. The example is an introduction to understanding how to determine the elastic and plastic bending moment of an Euler-Bernoulli cross-section. The example description is as follows:

A rigid horizontal element with a length of $6a$ is supported by a hinge at its mid-span. A couple of P forces are expected to be applied at both ends of the rigid component. With the interval of a from both ends, the element is supported by 6 rods. Rods are made from an elastic, perfectly plastic material. The yield limit of the material is 250MPa , and the elasticity modulus is 200GPa . The rods are with a diameter of 25mm with a length of 500mm . Assume the material is homogenous and has similar behavior in tension and compression. Also, we can ignore the effect of buckling in this example.

- Derive the compatibility equations.
- Determine the minimum required force P that the first bar(s) would yield.
- Determine the load P when the next bar(s) would yield.
- Determine the load P when the entire system becomes plastic¹.
- Sketch the Force P and its node displacement graph.



¹ This is the moment that the structure becomes a mechanism.

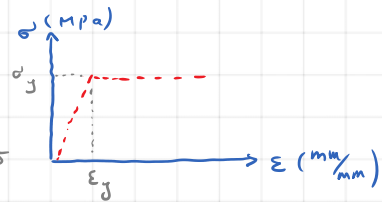


Elastic - perfectly plastic

$$\sigma_y = 250 \text{ MPa}$$

$$E = 200 \text{ GPa}$$

$$\epsilon_y = \frac{\sigma_y}{E} = 0.00125$$



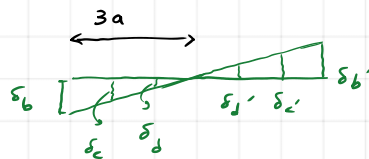
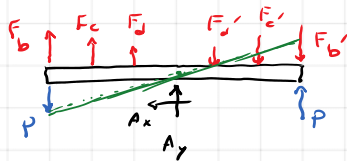
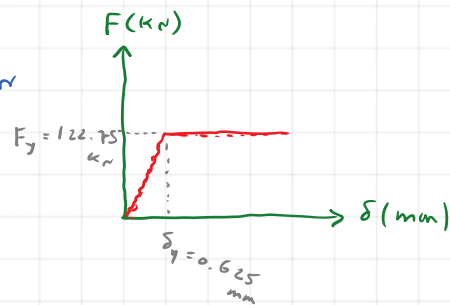
$$\sigma_y = 250 \text{ MPa}$$

$$A = \pi \frac{d^2}{4} = \pi \frac{(25 \text{ mm})^2}{4} = 491 \text{ mm}^2$$

$$\sigma = \frac{F}{A} \Rightarrow F_y = \sigma_y \cdot A = 250 \text{ MPa} \times 491 \text{ mm}^2 = 122.75 \text{ kN}$$

$$\delta_T = \frac{F_y \cdot L}{A E} = \frac{122.75 \text{ kN} \times 500 \text{ mm}}{491 \text{ mm}^2 \times 200 \text{ GPa}} = 0.625 \text{ mm}$$

$$\epsilon = \frac{\delta}{L} \rightarrow \delta_y = L \cdot \epsilon_y = 500 \text{ mm} \times 0.00125 = 0.625 \text{ mm}$$



$$\frac{\delta_b}{3a} = \frac{\delta_c}{2a} = \frac{\delta_d}{a}$$

$$\frac{\delta_{b'}}{3a} = \frac{\delta_{c'}}{2a} = \frac{\delta_{d'}}{a}$$

$$\left\{ \begin{array}{l} \delta_b = 3\delta_d \\ \delta_c = 2\delta_d \end{array} \right.$$

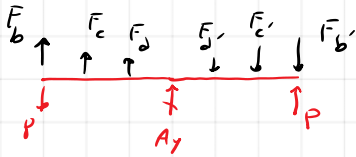
(set I)

$$\left\{ \begin{array}{l} \delta_{b'} = 3\delta_{d'} \\ \delta_{c'} = 2\delta_{d'} \end{array} \right.$$

$$\left\{ \begin{array}{l} \delta_b = \delta_{b'} \\ \delta_c = \delta_{c'} \\ \delta_d = \delta_{d'} \end{array} \right.$$

all bars in elastic phase: \rightarrow Elastic equation is valid.

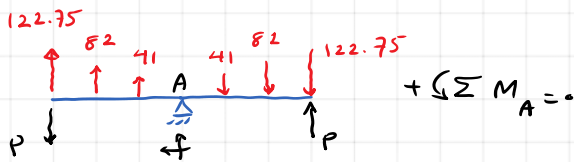
$$\delta = \frac{F \cdot L}{A \cdot E}, \quad \delta_b = \frac{F_b \cdot L}{A \cdot E}, \quad \delta_c = \frac{F_c \cdot L}{A \cdot E}, \quad \delta_d = \frac{F_d \cdot L}{A \cdot E}$$



Assume $F_b = F_b' = F_y = 122.75 \text{ kN}$

(Set I) $\rightarrow \delta_b = 3\delta_d \rightarrow \frac{F_b \cdot L}{AE} = 3 \frac{F_d \cdot L}{AE} \rightarrow F_d = \frac{1}{3} F_b \rightarrow F_d = \frac{1}{3} \times 122.75 \approx 41 \text{ kN} < F_y$

$\delta_c = 2\delta_d \rightarrow \frac{F_c \cdot L}{AE} = 2 \frac{F_d \cdot L}{AE} \rightarrow F_c = 2F_d \rightarrow F_c \approx 82 \text{ kN} < F_y = 122.75 \text{ kN}$



$$P \cdot (3a) + P \cdot (3a) - 122.75 \times (3a) \times 2 - 82 \times (2a) \times 2 - 41 \times (a) \times 2 = 0$$

$$\rightarrow P = 191 \text{ kN}$$

①

$$F_b = F_y = 122.75 \text{ kN} \rightarrow \delta_b = \delta_y = 0.625 \text{ mm}$$

$$\sigma_b = \sigma_y = 250 \text{ MPa} \rightarrow \epsilon_b = \epsilon_y = 0.00125$$

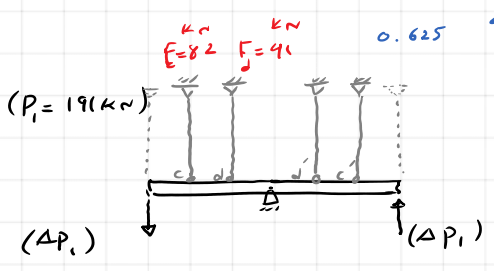
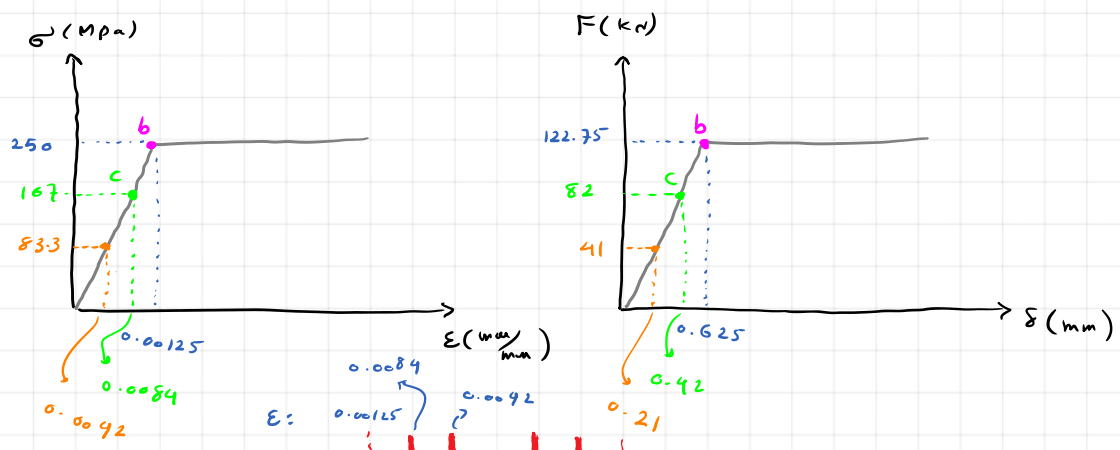
(c), $F_c = 82 \text{ kN} \rightarrow \delta_c = \frac{F \cdot L}{AE} = \frac{82 \text{ kN} \times 500 \text{ mm}}{491 \text{ mm}^2 \times 200 \text{ GPa}} = 0.42 \text{ mm}$,

$$\rightarrow \sigma = \frac{F}{A} = \frac{82000 \text{ N}}{491 \text{ mm}^2} = 167 \text{ MPa}$$

$$\epsilon = \frac{\sigma}{E} = \frac{167 \text{ MPa}}{200 \text{ GPa}} = 0.00084$$

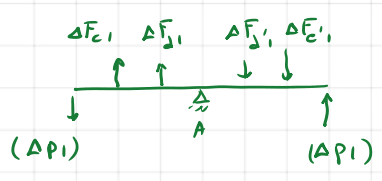
d), $F_d = 41 \text{ kN}$, $\delta_d = 0.21 \text{ mm}$, $\sigma = 83.3 \text{ MPa}$, $\epsilon = 0.00042$

- (-) (b)
- (-) (c)
- (-) (d)



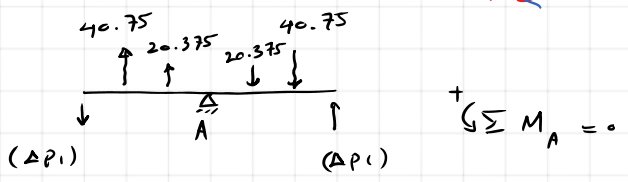
capacity left for element c $\rightarrow 122.75 - 82 = 40.75 \text{ kN}$
 " " " " d $\rightarrow 122.75 - 41 = 81.75 \text{ kN}$

$P_0 = 191 \text{ kN}$



Assume c & c' become plastic before d & d'.
 $\Delta F_{c1} = 40.75 \text{ kN}$

(Set I) $\rightarrow \delta_c = 2 \delta_d \rightarrow \frac{F_c \cdot L}{AE} = 2 \frac{F_d \cdot L}{AE} \rightarrow (\Delta F_{d1}) = \frac{(\Delta F_{c1})}{2} = 20.375 \text{ kN} \leq 81.75 \text{ kN}$ (OK)



$(\Delta P_1) \cdot 3a - 2 - 40.75 \times 2a \times 2 - 20.375 \times a \times 2 = 0 \Rightarrow (\Delta P_1) \leq 34 \text{ kN}$

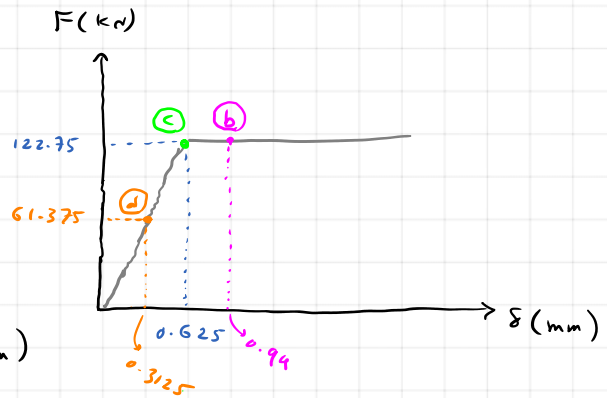
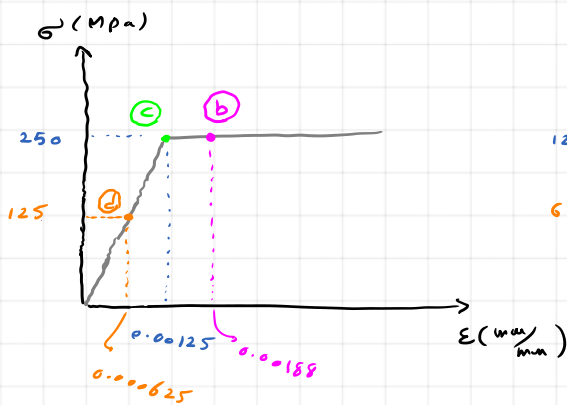
$F_c = (F_{c1}) + (\Delta F_{c1}) = 122.75 \text{ kN} \rightarrow \delta_c = 0.625 \text{ mm}$

$F_d = (F_{d1}) + (\Delta P_{d1}) = 41 + 20.375 = 61.375 \text{ kN} \rightarrow \delta_d = \frac{F_d \cdot L}{AE} = \frac{61.375 \text{ kN} \times 500 \text{ mm}}{491 \text{ mm}^2 \times 200 \text{ GPa}} = 0.3125 \text{ mm}$

(b) $\rightarrow F_b = 122.75 \text{ kN}, \delta_b = 3\delta_d = 0.94 \text{ mm} > \delta_y = 0.625 \text{ mm}$

Not valid ($\epsilon > \frac{\sigma_y}{E}$)
 $\epsilon = \frac{\delta}{L} = \frac{0.94 \text{ mm}}{500 \text{ mm}} = 0.00188 > \epsilon_y = 0.00125$

- (-) (b)
- (-) (c)
- (-) (d)

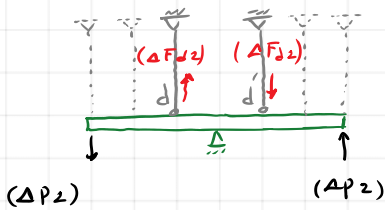


$$P_2 = P_1 + \Delta P_1 = 191 \text{ kN} + 34 \text{ kN} = 225 \text{ kN}$$

$$P = P_{(1)} = 191 \text{ kN}, \delta_b = 0.625 \text{ mm}$$

$$P = P_{(2)} = 225 \text{ kN}, \delta_b = 0.94 \text{ mm}$$

$$F_d = 61.375 \text{ kN}$$



$$(\Delta F_{d2}) = 122.75 \text{ kN} - 61.375 \text{ kN} = 61.375 \text{ kN}$$

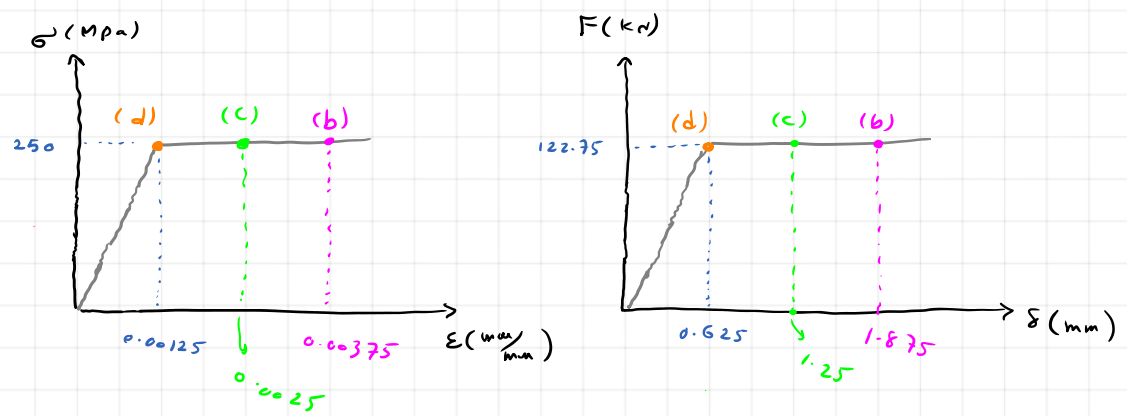
$$+\circlearrowleft \sum M_A = 0 \rightarrow (\Delta P_2) \cdot 3a \cdot 2 - (\Delta F_{d2}) \cdot a \cdot 2 = 0 \rightarrow (\Delta P_2) \cong 20.5 \text{ kN}$$

$$F_d + \Delta F_{d2} \quad (\Delta F_{d2})$$

$$F_d = 61.375 + 61.375 = 122.75 \text{ kN} \rightarrow \delta_d = 0.625, \epsilon_d = 0.00125, \sigma_d = \sigma_y = 250 \text{ MPa}$$

$$c \ \& \ b \rightarrow \begin{cases} F_b = 122.75 \text{ kN} \\ F_c = 122.75 \text{ kN} \end{cases} \quad \begin{aligned} \delta_b &= 3\delta_d = 3 \times 0.625 \text{ mm} = 1.875 \text{ mm}, \epsilon = \frac{\delta}{L} = 0.00375 \gg 0.00125 \\ \delta_c &= 2\delta_d = 2 \times 0.625 \text{ mm} = 1.25 \text{ mm}, \epsilon = \frac{\delta}{L} = 0.0025 \gg 0.00125 \end{aligned}$$

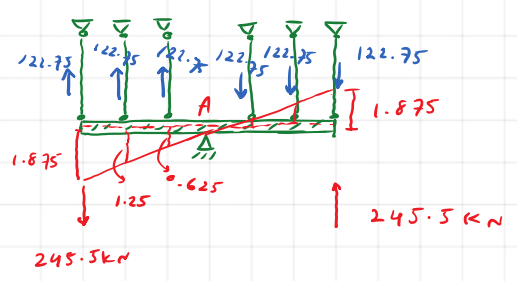
- (→) (b)
- (-) (c)
- (-) (d)



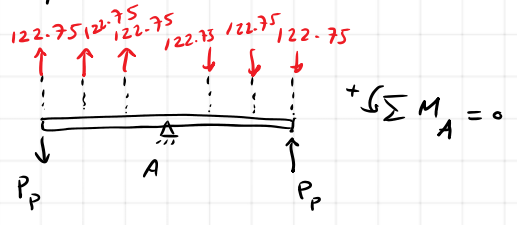
$(\Delta P_2) = 20.5 \text{ kN}$

$P_3 = P_2 + \Delta P_2 = 225 \text{ kN} + 20.5 \text{ kN} = 245.5 \text{ kN}$

$\delta_b = 1.875 \text{ mm}$



Determine the plastic load of the shown system:



$P_p \times 3a \times 2 - 122.75 \times 3a \times 2 - 122.75 \times 2a \times 2 - 122.75 \times a \times 2 = 0 \rightarrow P_p = 245.5 \text{ kN}$

